



Cold Spray Aluminum for Magnesium Gearbox Repair

Phillip F. Leyman

US Army Research Laboratory

Weapons & Materials Research Directorate

SERDP/ESTCP Surface Finishing Workshop

February 26-28, 2008

Report Documentation Page				Form Approved OMB No. 0704-0188	
Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.					
1. REPORT DATE FEB 2008		2. REPORT TYPE		3. DATES COVERED 00-00-2008 to 00-00-2008	
4. TITLE AND SUBTITLE Cold Spray Aluminum for Magnesium Gearbox Repair				5a. CONTRACT NUMBER	
				5b. GRANT NUMBER	
				5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S)				5d. PROJECT NUMBER	
				5e. TASK NUMBER	
				5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U. S. Army Research Laboratory, Weapons & Materials Research Directorate, Aberdeen Proving Ground, MD, 21005				8. PERFORMING ORGANIZATION REPORT NUMBER	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)				10. SPONSOR/MONITOR'S ACRONYM(S)	
				11. SPONSOR/MONITOR'S REPORT NUMBER(S)	
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution unlimited					
13. SUPPLEMENTARY NOTES Surface Finishing and Repair Issues for Sustaining New Military Aircraft Workshop, February 26-28, 2008, Tempe, AZ. Sponsored by SERDP/ESTCP.					
14. ABSTRACT					
15. SUBJECT TERMS					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT Same as Report (SAR)	18. NUMBER OF PAGES 42	19a. NAME OF RESPONSIBLE PERSON
a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified			



ESTCP Program Goal

ESTCP Proposal 06-E-PP3-031

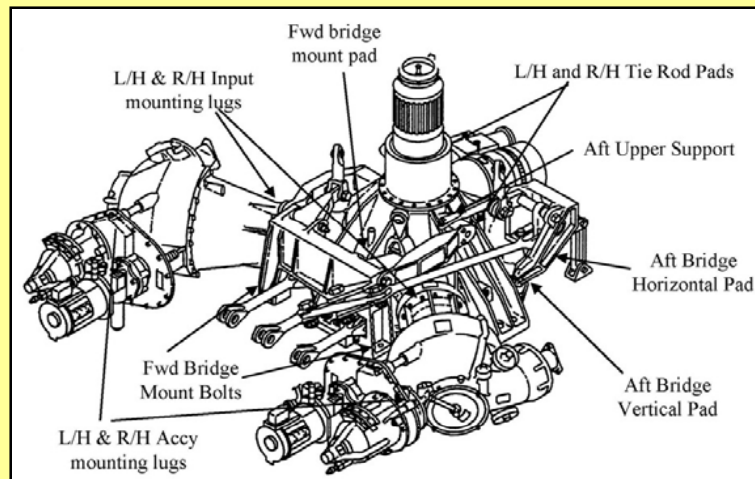
- To reclaim Magnesium alloy components on Army and Navy helicopters that have been removed from service due to severe corrosion and/or wear.
- ARL will provide a repair/rebuild Cold Spray procedure for scrapped parts and assist in the transition and implementation of this technology, initially, at NADEP, Cherry Point, NC.



Problems With Current Surface Treatment Methods



- Exposure to hexavalent chrome is hazardous to workers' health. OSHA limits on chromium exposure are becoming increasingly stringent.
- Even with chromated surface treatments, Mg components suffer severe degradation in service
- Most corrosion occurs at mating pads, supports, and mounting lugs where dissimilar metal is in contact with Mg; damage is most likely to occur in those locations as well



H-60 Main Transmission Housing showing areas most susceptible to corrosion



Corrosion on H-53 Tail Gearbox Housing



Program Objectives

- **Develop the densest, thinnest, most corrosion resistant Aluminum-based Cold Spray coating with the greatest adhesive bond strength to Magnesium.**
- **Determine effects of feedstock material and process parameters on coating thickness, microstructure, adhesion, and corrosion performance for the Cold Spray coatings on Magnesium substrates.**



*Joint Test Protocol (JTP)
has been developed*

U.S. DEPARTMENT OF DEFENSE
Environmental Security Technology Certification Program
(ESTCP)

JOINT TEST PROTOCOL

*Supersonic Particle Deposition Technology for
Repair of Magnesium Aircraft Components*

Date: October 2, 2006

Prepared By:
Hard Chrome Alternatives Team (HCAAT)





ARL Leveraged Formal Programs



Develop aluminum cold spray coatings for aluminum, magnesium and/or steel substrates have been established with the following:

- 1. Defense Science & Technology Organization (DSTO)**
- 2. Joint Strike Fighter (JSF)**
- 3. National Center for Manufacturing Sciences (NCMS)**
- 4. Lockheed Martin**
- 5. Penn State Applied Research Laboratory**
- 6. Lawrence Livermore National Labs (LLNL)**
- 7. South Dakota School of Mines (SDSM)**



**Cold Spray Center at the
US Army Research Laboratory (ARL)
Aberdeen Proving Ground, MD 21005-5069**



ARL Cold Spray Research Team

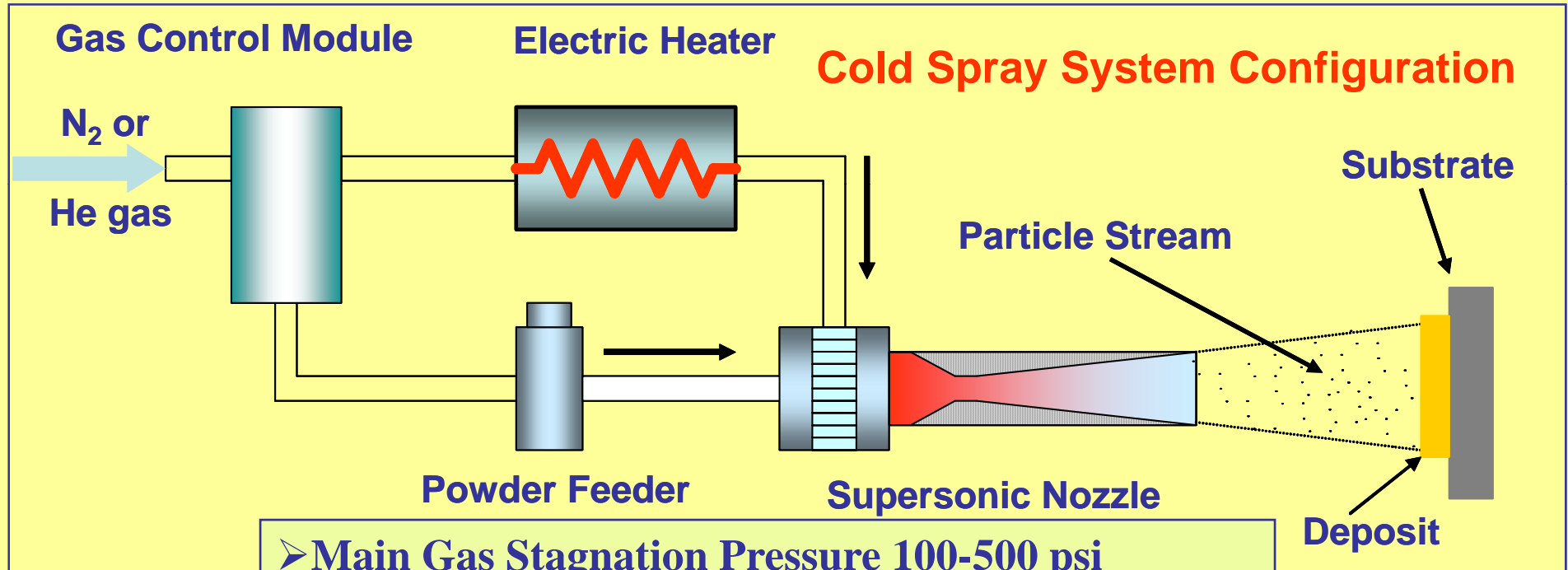
Victor Champagne	Team Lead	(410) 306-0822
Phillip Leyman	Process Engineer	(410) 306-0818
Dr. Dennis Helfritch	Modeling/Simulation	(410) 306-1928
Dr. Matthew Trexler	Materials Engineer	(410) 306-1592
Michael Lister	Materials Engineer	(410) 306-0808
Carl Paxton	Process Technician	(410) 306-2026
Marc Pepi	Mechanical Engineer	(410) 306-0848



Overview of Cold Spray Technology



Cold Spray: a process by which particulates are deposited by means of ballistic impingement upon a suitable substrate at super sonic velocities to form a coating or a free-standing structure.



- Main Gas Stagnation Pressure 100-500 psi
- Gas Temperature 0-500°C
- Main Gas Flow Rate 30-100 CFM
- Powder Feed Rate 1 to 10 pounds/hour
- Particle Velocity 300-1500 m/sec.
- Particle Size 1-100µm diameter



Stationary Cold Spray System at ARL



Robot-Controlled, High Pressure, He and N Gas





Cold Spray Advantages



Mechanical mixing bond at substrate interface

plastic deformation may disrupt thin oxide surface films to permit bonding similar to explosive welding

Compressive residual stresses

particles “peen” surface

plasma and wire-arc thermal spray coatings tend to be in tension

High density

low porosity: $< 0.5\%$

low oxide content $< 0.3\%$

Thick coatings

free-form fabrication

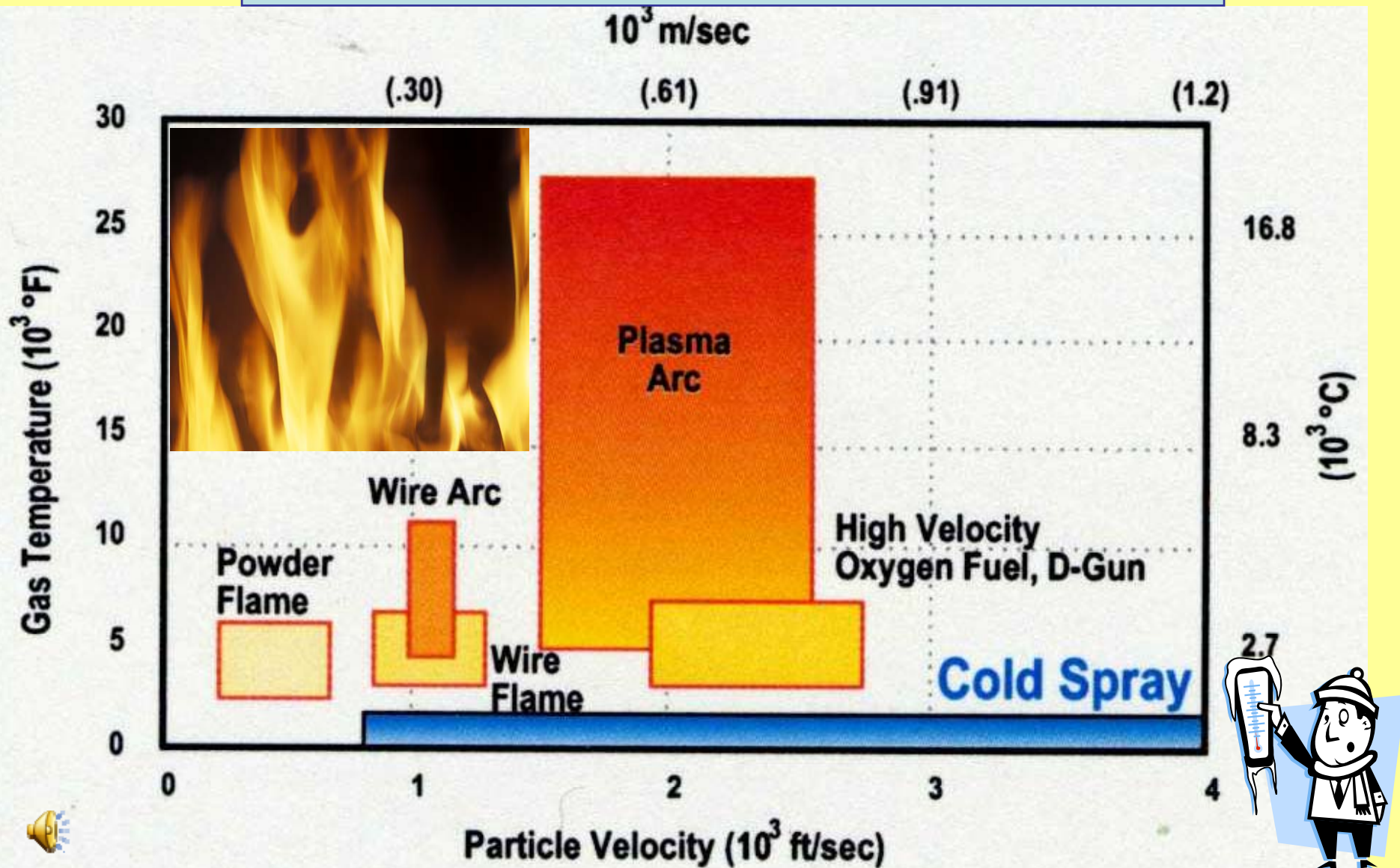
Low Temperature Application

thermally sensitive substrates

low stresses due to CTE mismatch



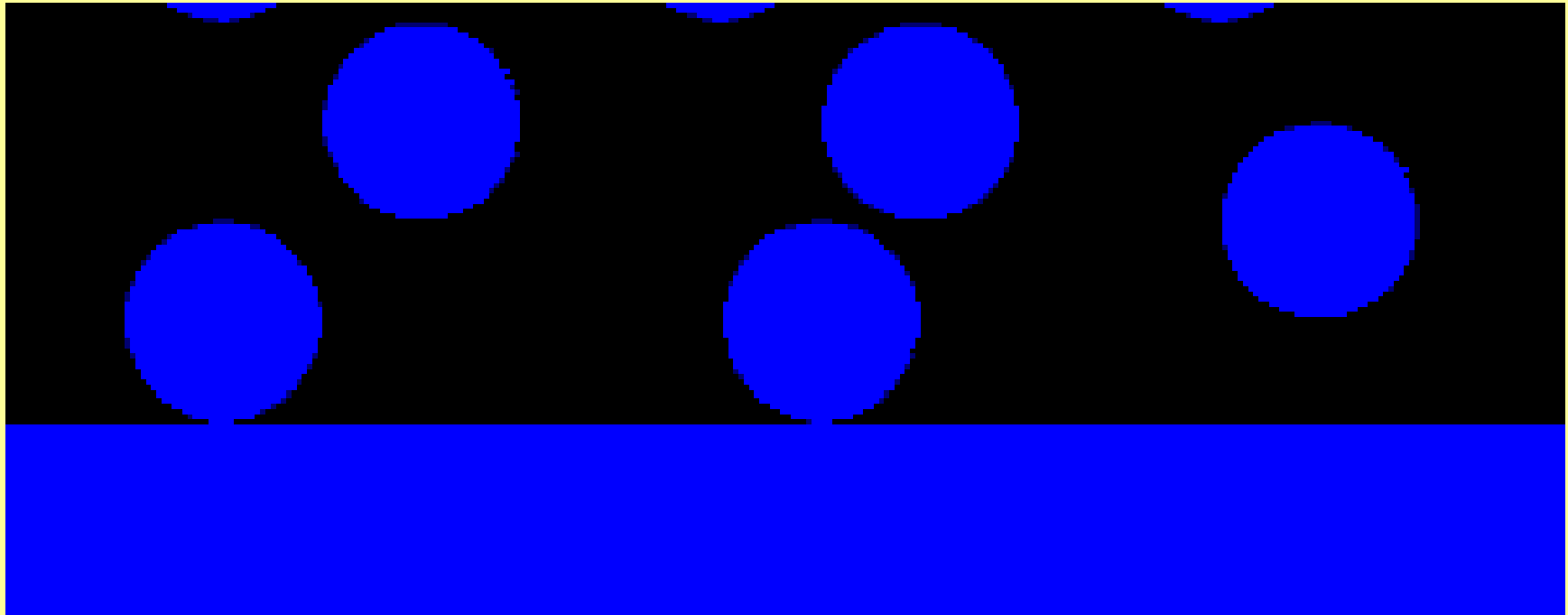
Cold Spray vs. Thermal Spray



Cold Spray is performed at lower temperatures at high particle velocities



Particle/Substrate Interaction*

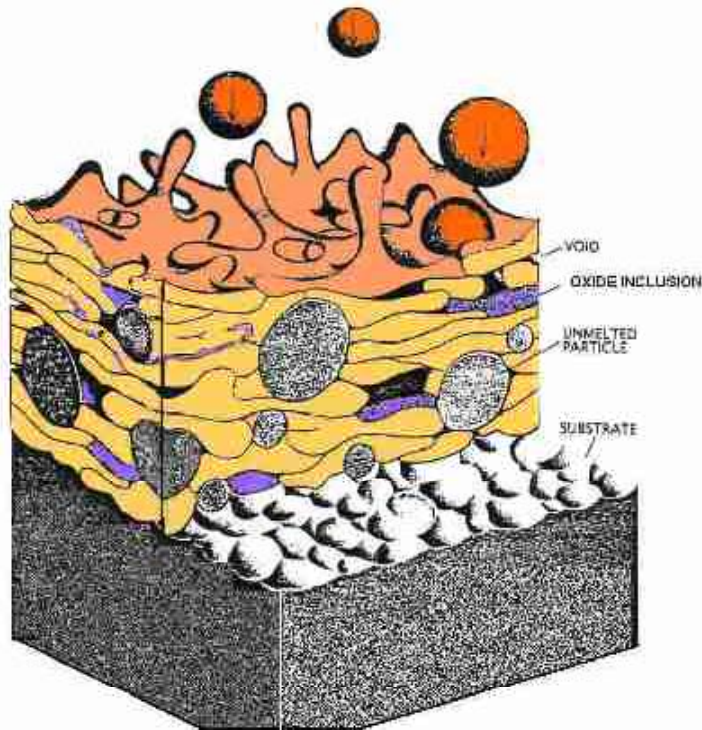


*from H. Assadi, www.modares.ac.ir/eng/ha10003/CGS.htm



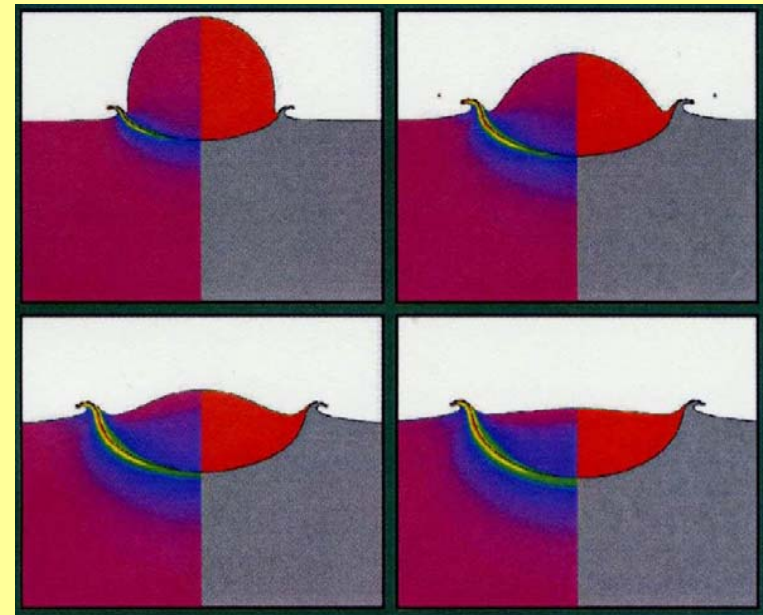
Advantages of Low Temperature Process

Thermal Spray



www.gordonengland.co.uk

Cold Spray



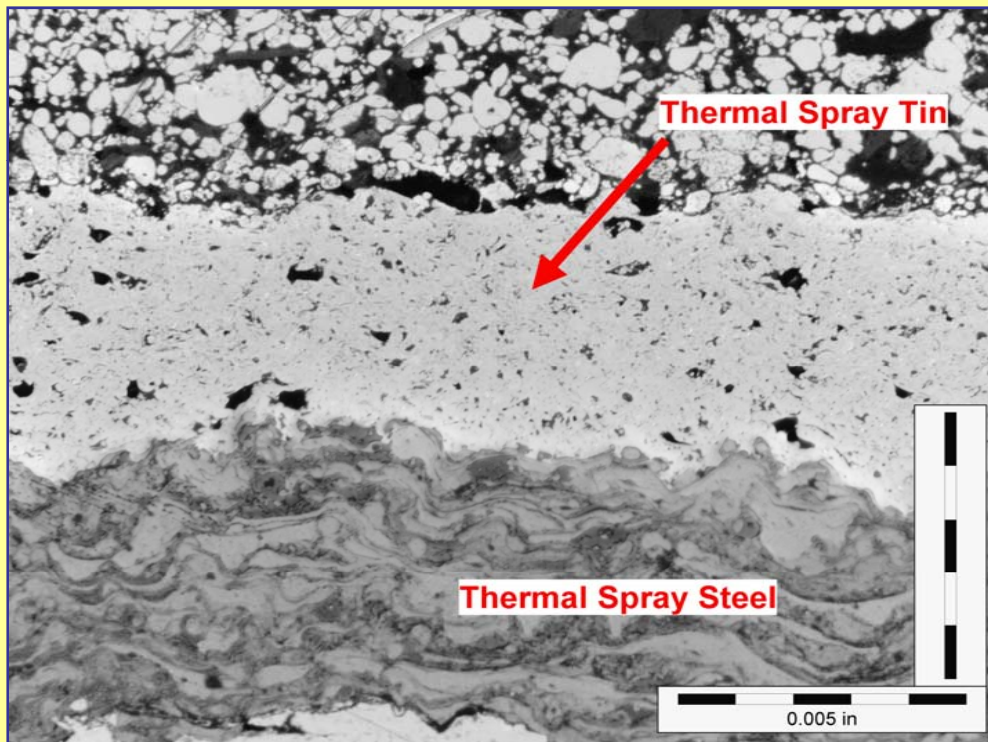
The melting of particles that occurs during most thermal spray processes can result in oxidation of both the coating and substrate materials. The resulting oxides decrease the adhesive and cohesive strengths of the coating. The cold spray process avoids such reactions.



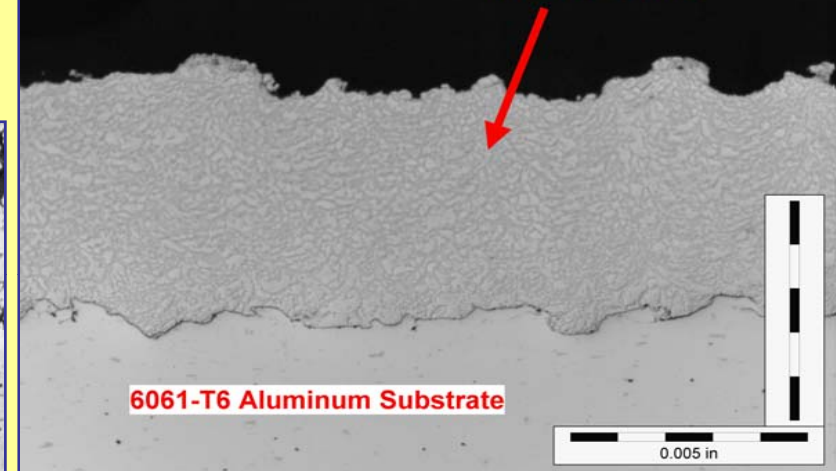
Cold Spray vs. Thermal Spray



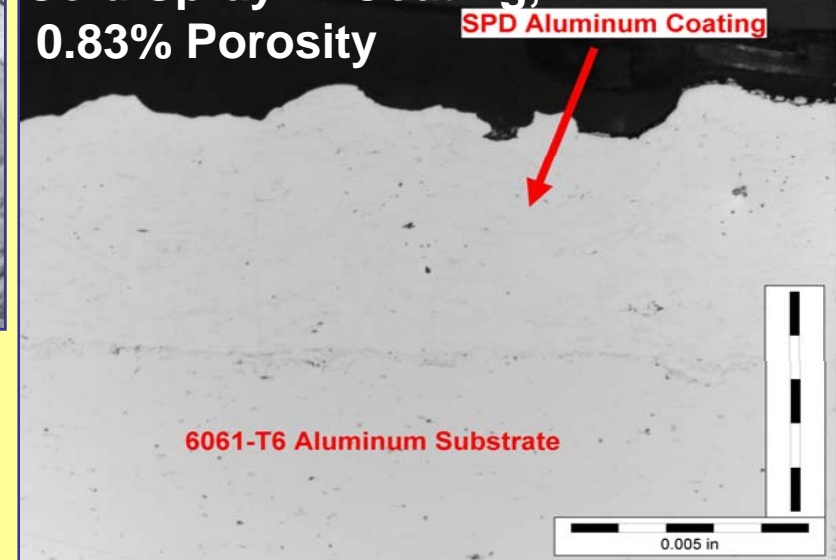
**Flame Spray Sn & Steel
Coating, 12.2% Porosity**



**Cold Spray Sn Coating,
0% Porosity**

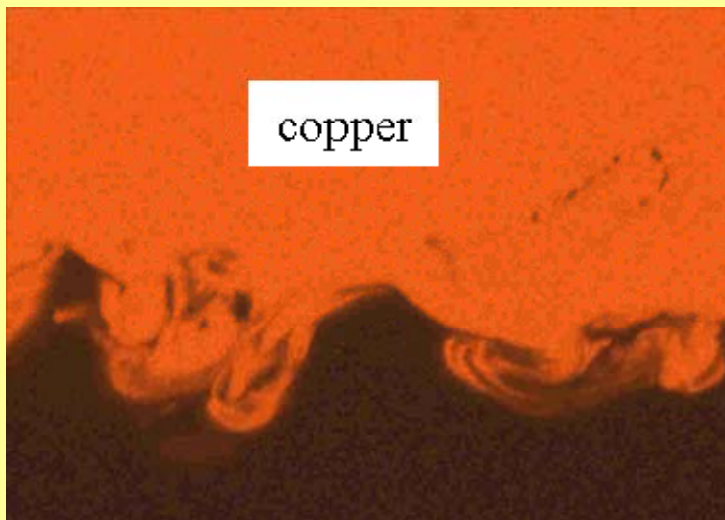
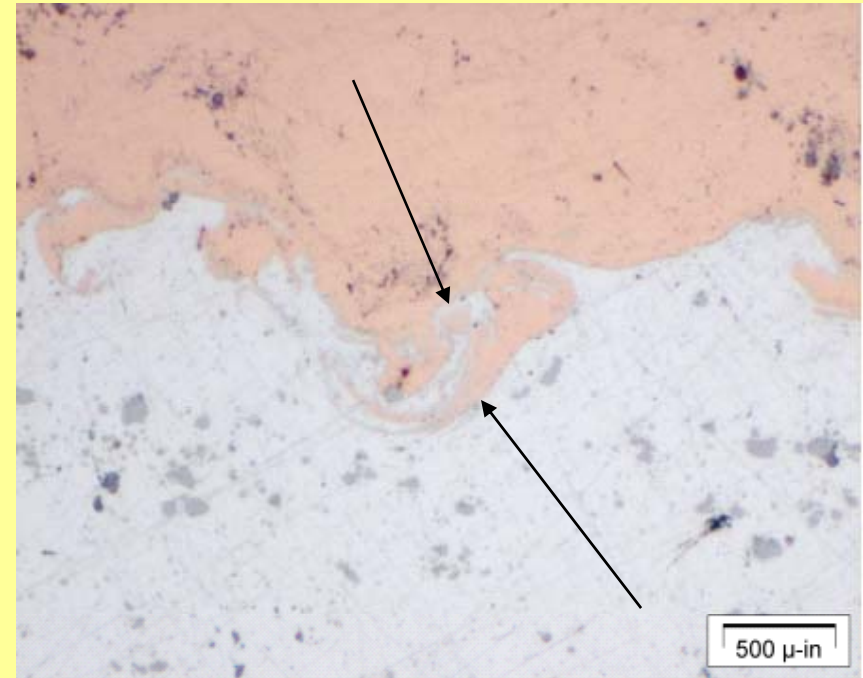
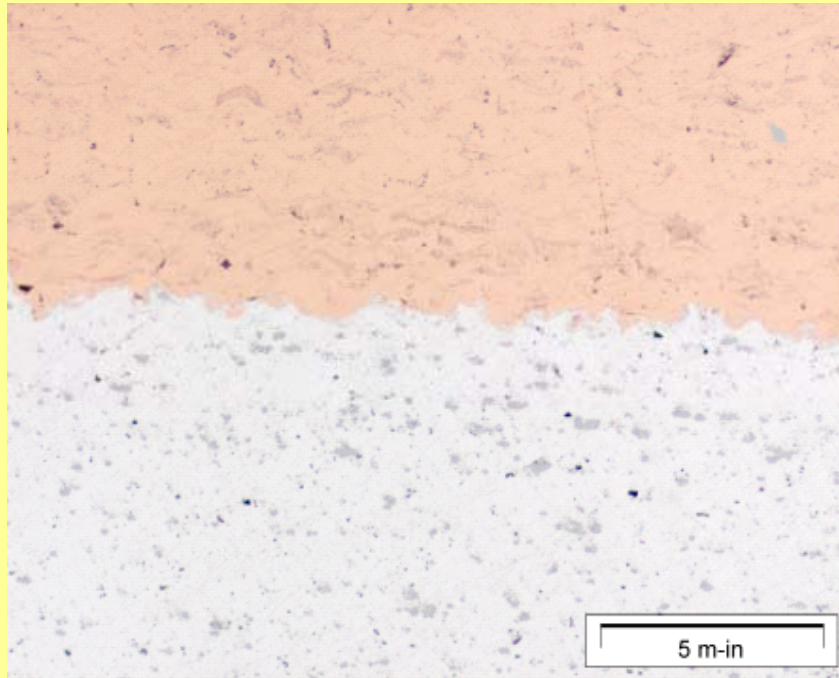


**Cold Spray Al Coating,
0.83% Porosity**



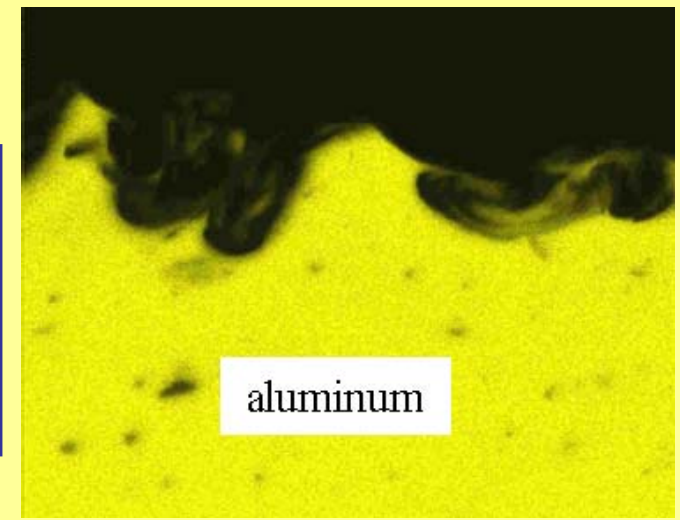


Mechanical Mixing at Interface



copper

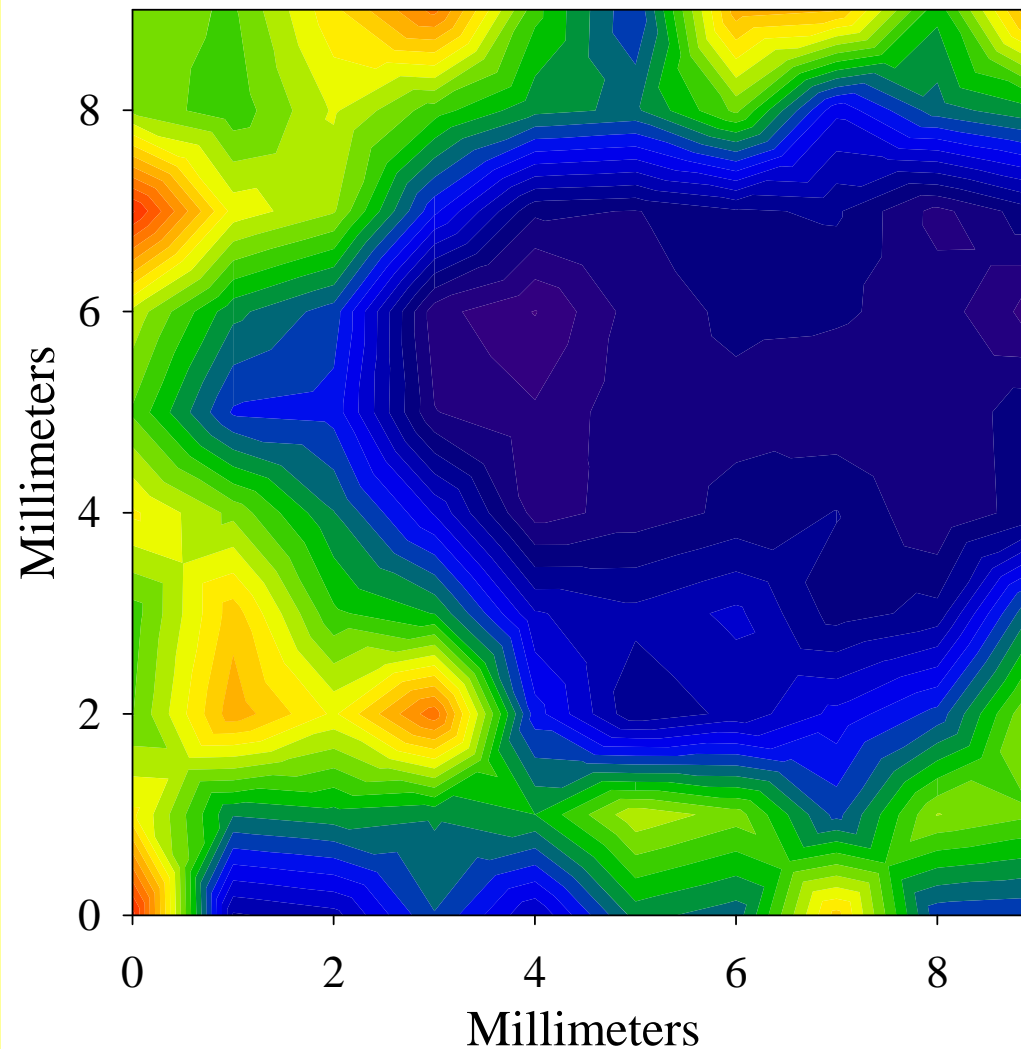
EDS X-ray Mapping
showing mechanical
mixing between
coating material and
substrate



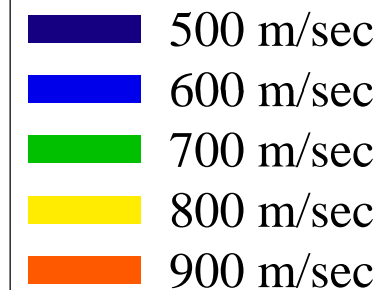
aluminum



Particle Velocity Distribution Measured by DPV 2000



**20 micron copper particles
25 mm downstream
400 psi, 400 C N₂ gas**





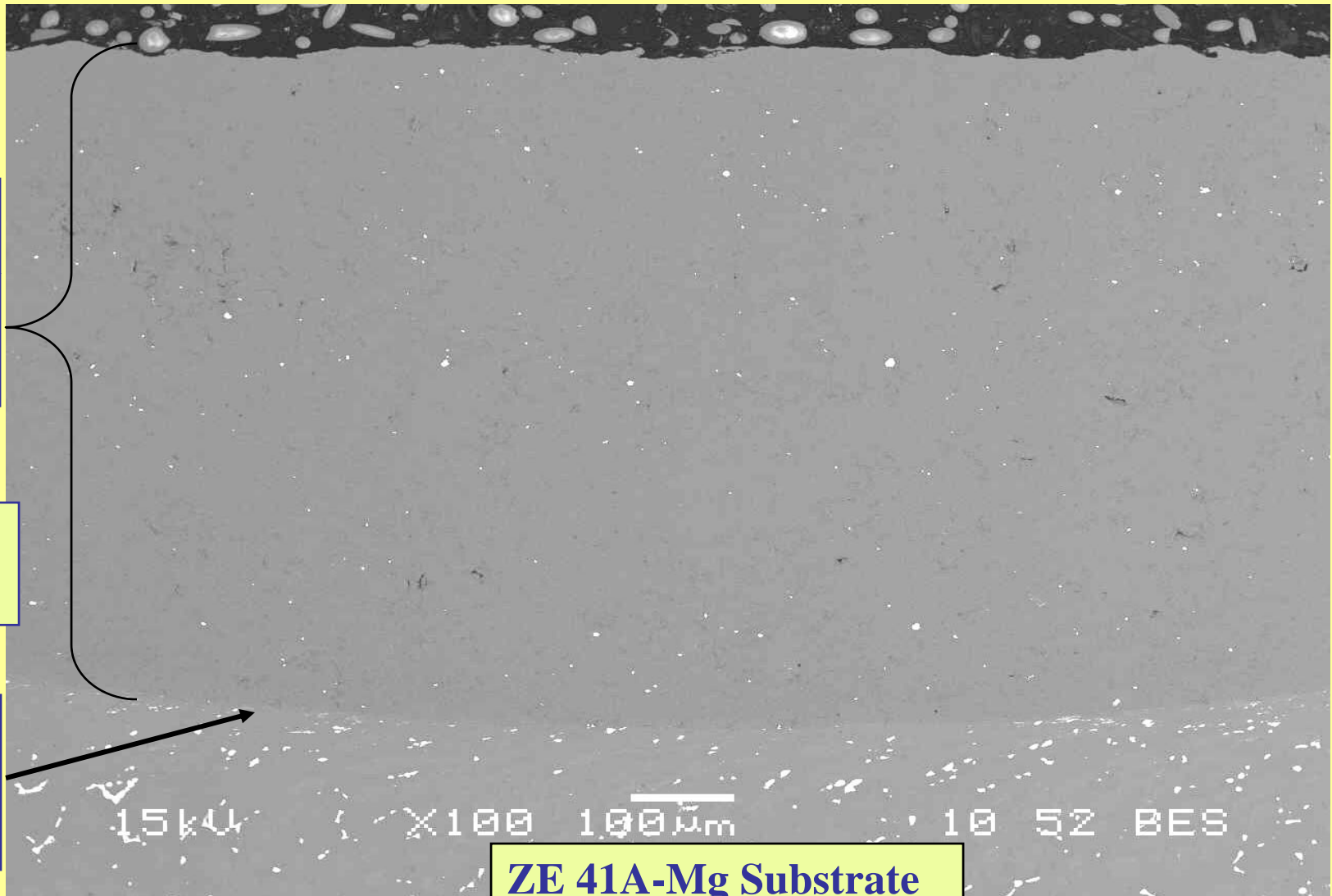
Cold Spray Coating of CP-Al On ZE 41A-Mg (Helium Carrier Gas)

**~100%
Dense**

**Cold
Spray
CP- Al
Coating**

**8,500 psi
adhesion**

**Coating /
Substrate
Interface**



ZE 41A-Mg Substrate

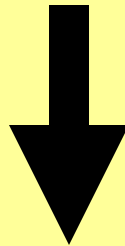


ARL Technical Hurdle

No Porosity & 8,500 psi bond strength using Helium

Achieve similar results with the use of nitrogen as the carrier gas

Technical Approach

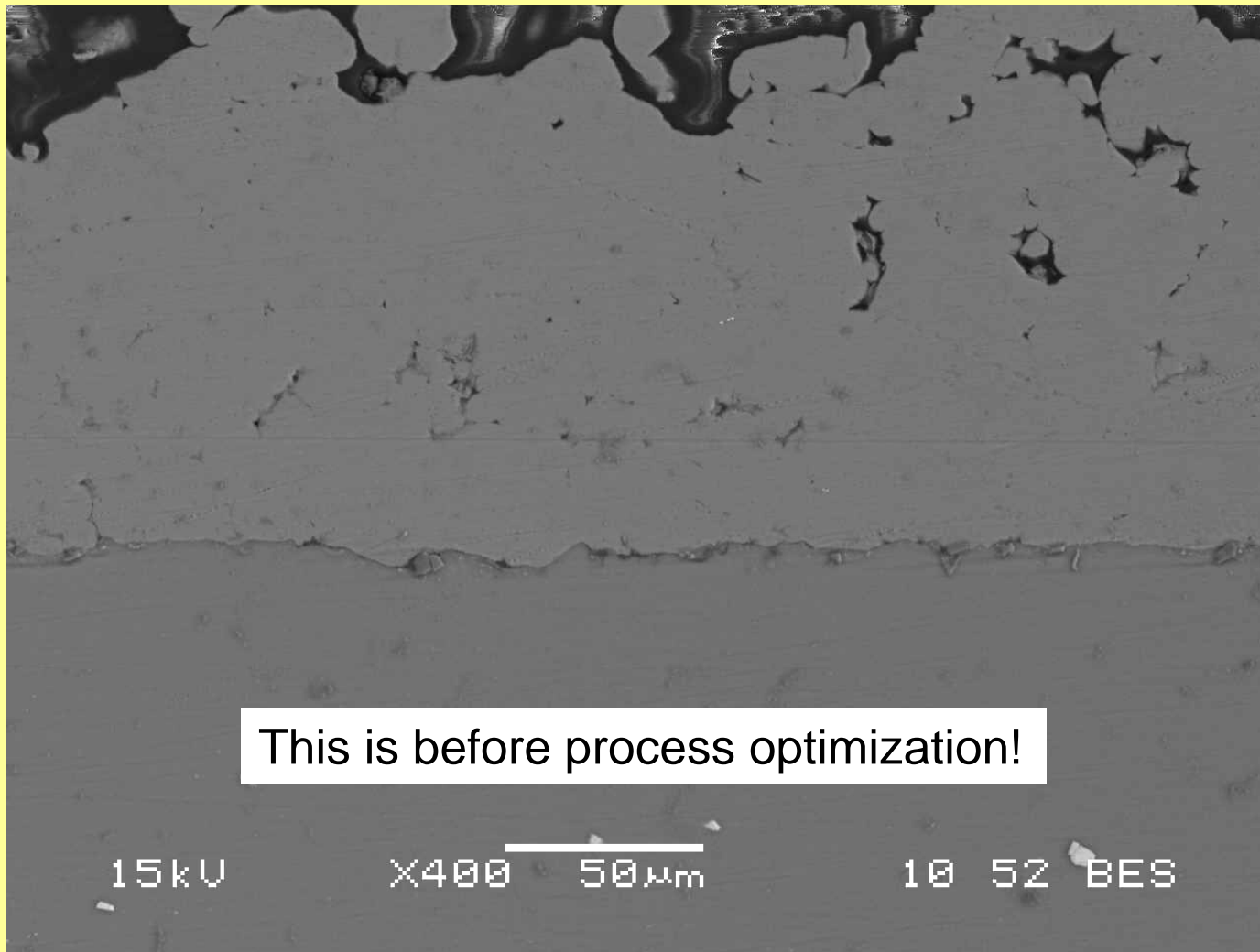


- Nozzle – Material & Design
- Powder Size, Morphology
- Process Parameters





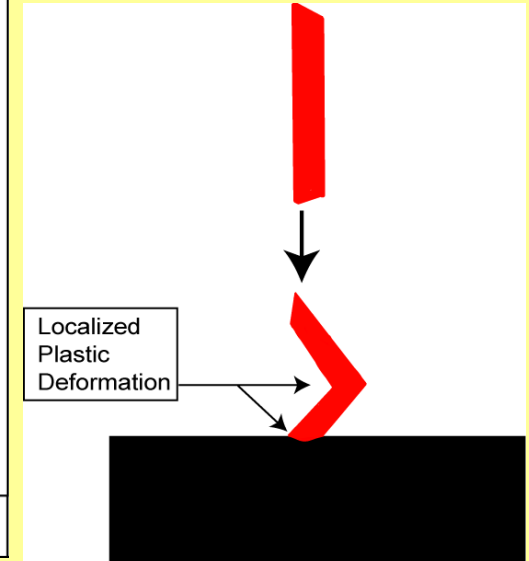
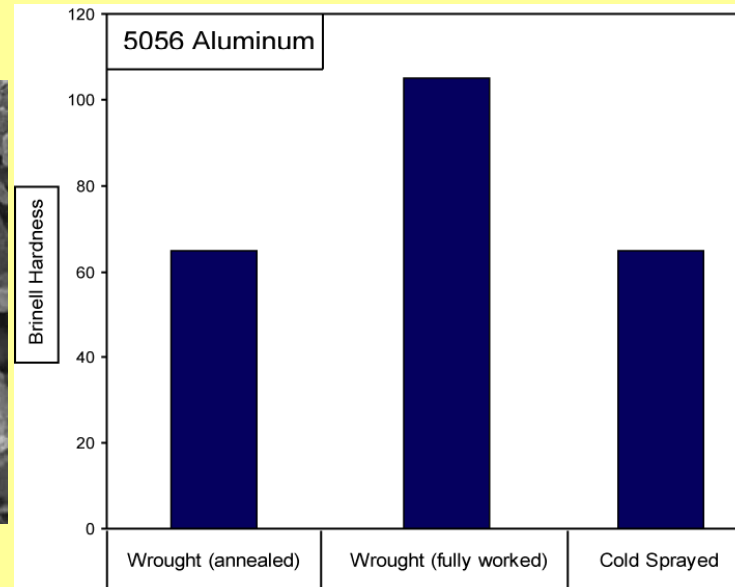
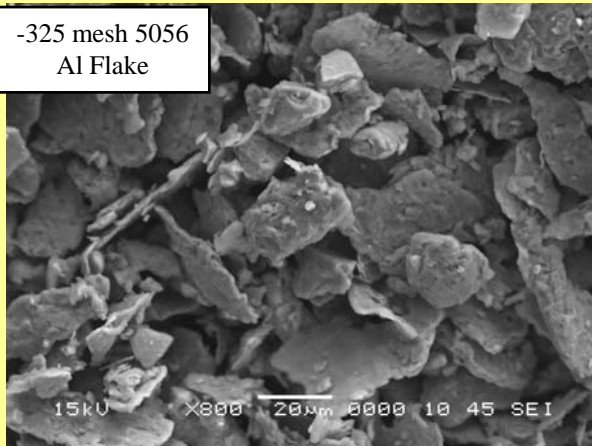
Cold Spray Coating of CP-Al on ZE41A-Mag (Nitrogen at 380 psi, 250 C)



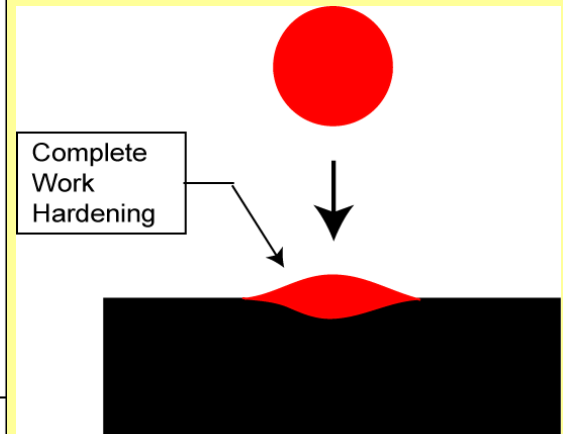
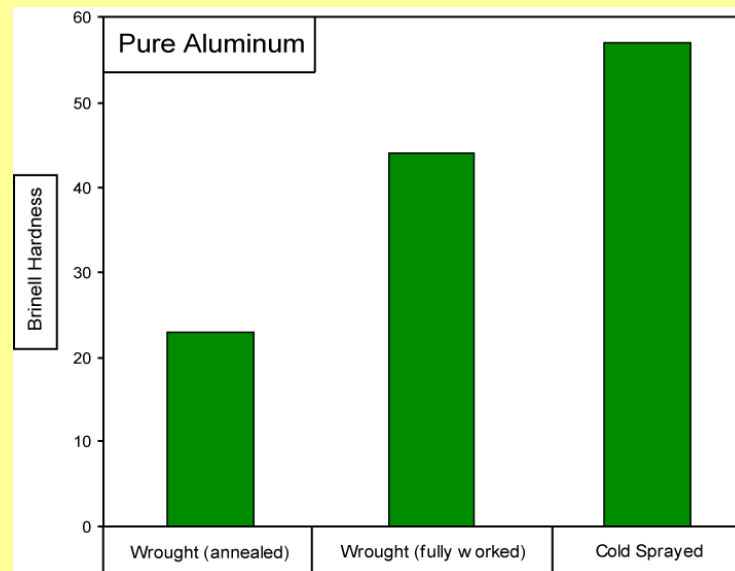
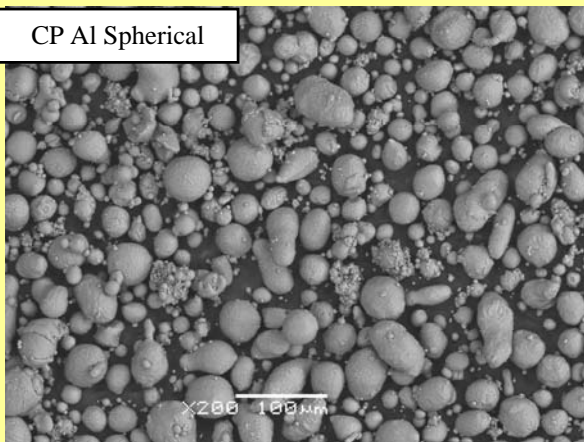


Aluminum Powder Morphology

-325 mesh 5056
Al Flake

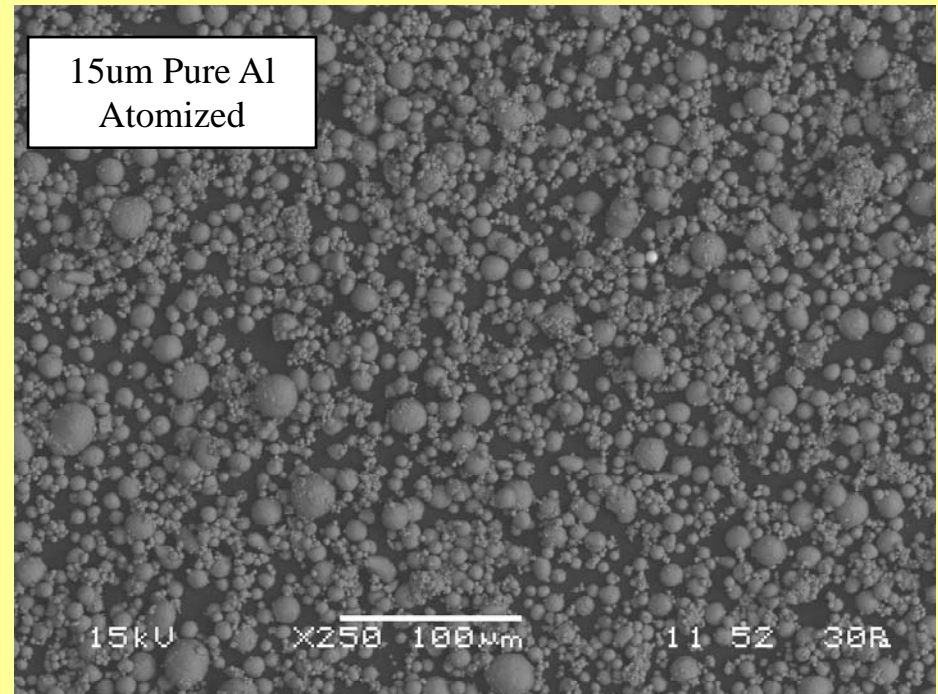


CP Al Spherical





Aluminum Powder Morphology



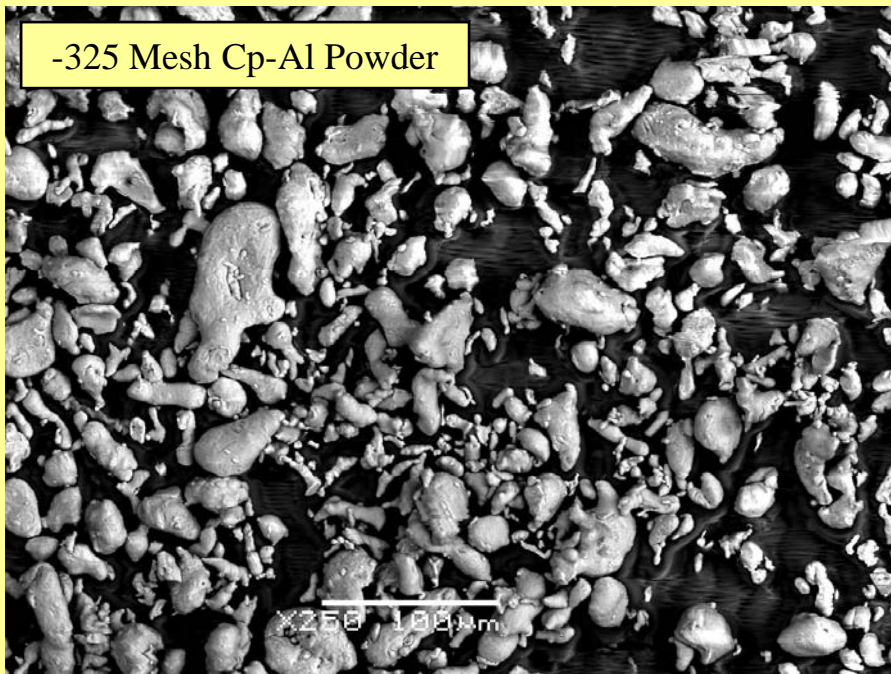
Coating quality is critically dependent on the feed powder composition, morphology, oxygen content, and mechanical properties.



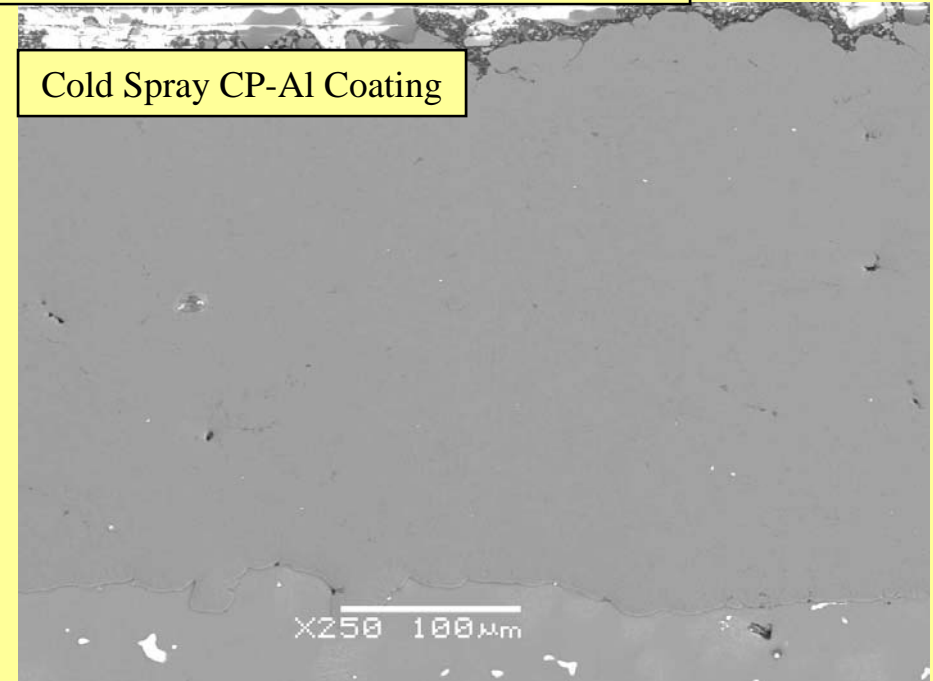
Purity of Cold Sprayed Aluminum



Oxygen content measured by Inert Gas Fusion
ASTM E 1019-03



0.34 %Oxygen



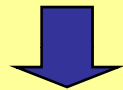
0.25 %Oxygen

*The oxygen content of the cold spray coating is largely determined by the oxygen content of the original powder, not the process.

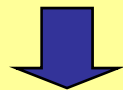


Modeling Efforts

Gasdynamic equations are used to calculate gas velocity and temperature within the nozzle and downstream of the nozzle exit.



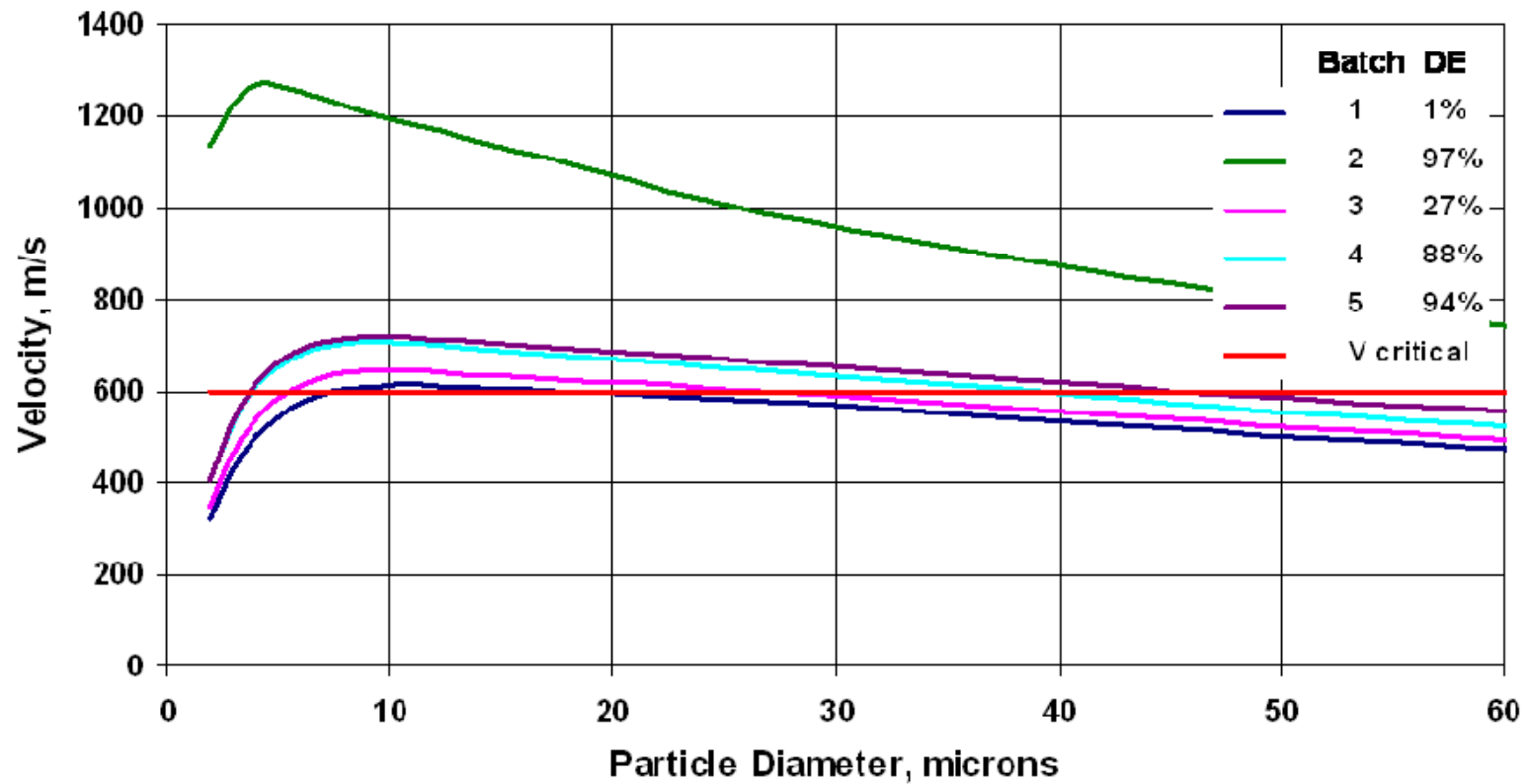
The resulting particle velocities and temperatures are then calculated by gas-particle drag and heat transfer.



The log normal particle size distribution is integrated from the smallest diameter to the largest diameter for those particles with velocities greater than the critical velocity, to determine DE.



Particle Velocity & Deposition Efficiency



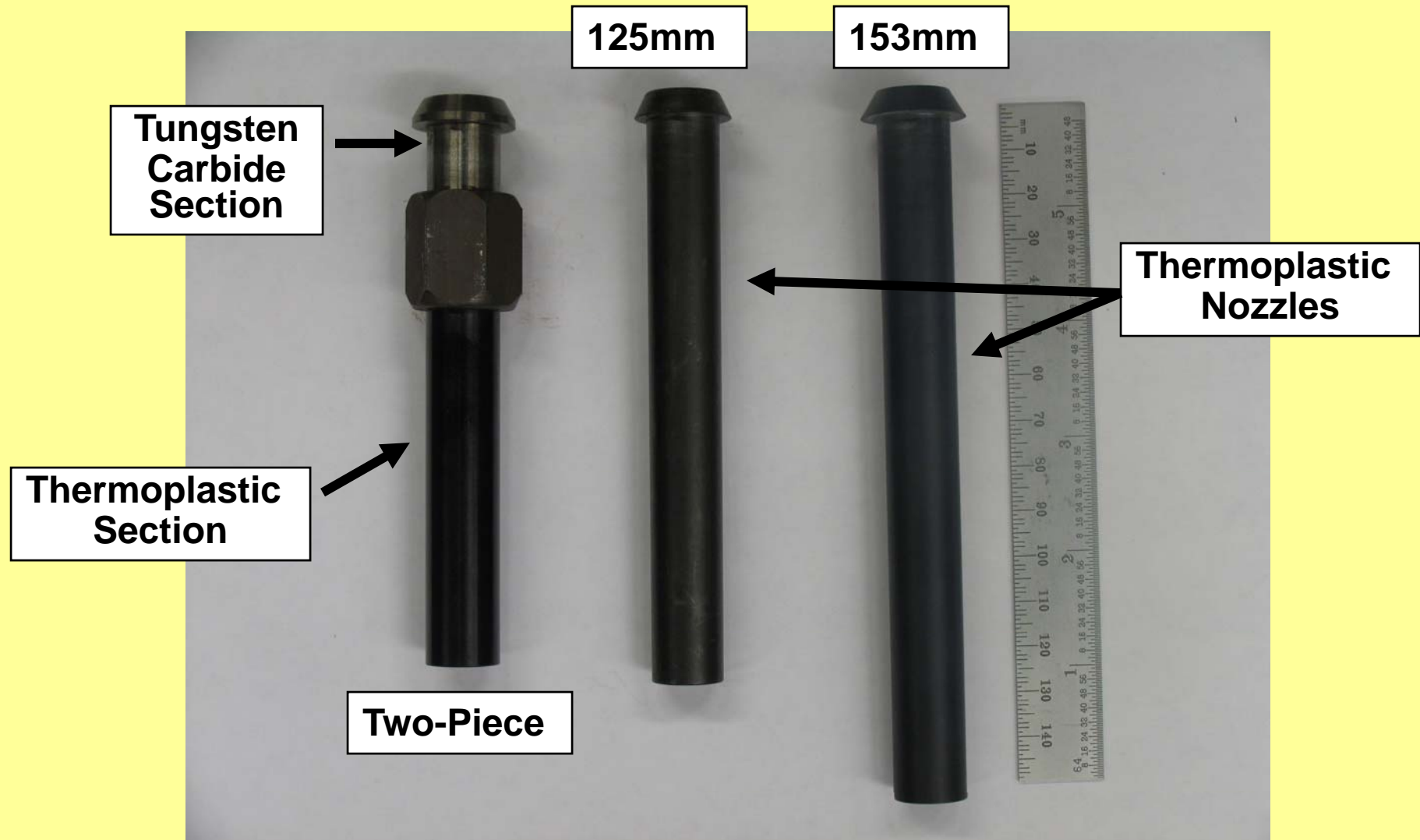


Nozzle Designs

Material	Length (mm)	Process Conditions	Particle Velocity
Tungsten Carbide	115	He, 380psi, RT	1020
Tungsten Carbide	115	N2, 380psi, 250C	590
WC/ Thermoplastic	115	N2, 380psi, 300C	605
Thermoplastic	125	N2, 380psi, 400C	690
Thermoplastic	153	N2, 380psi, 400C	710



Thermoplastic Cold Spray Nozzles

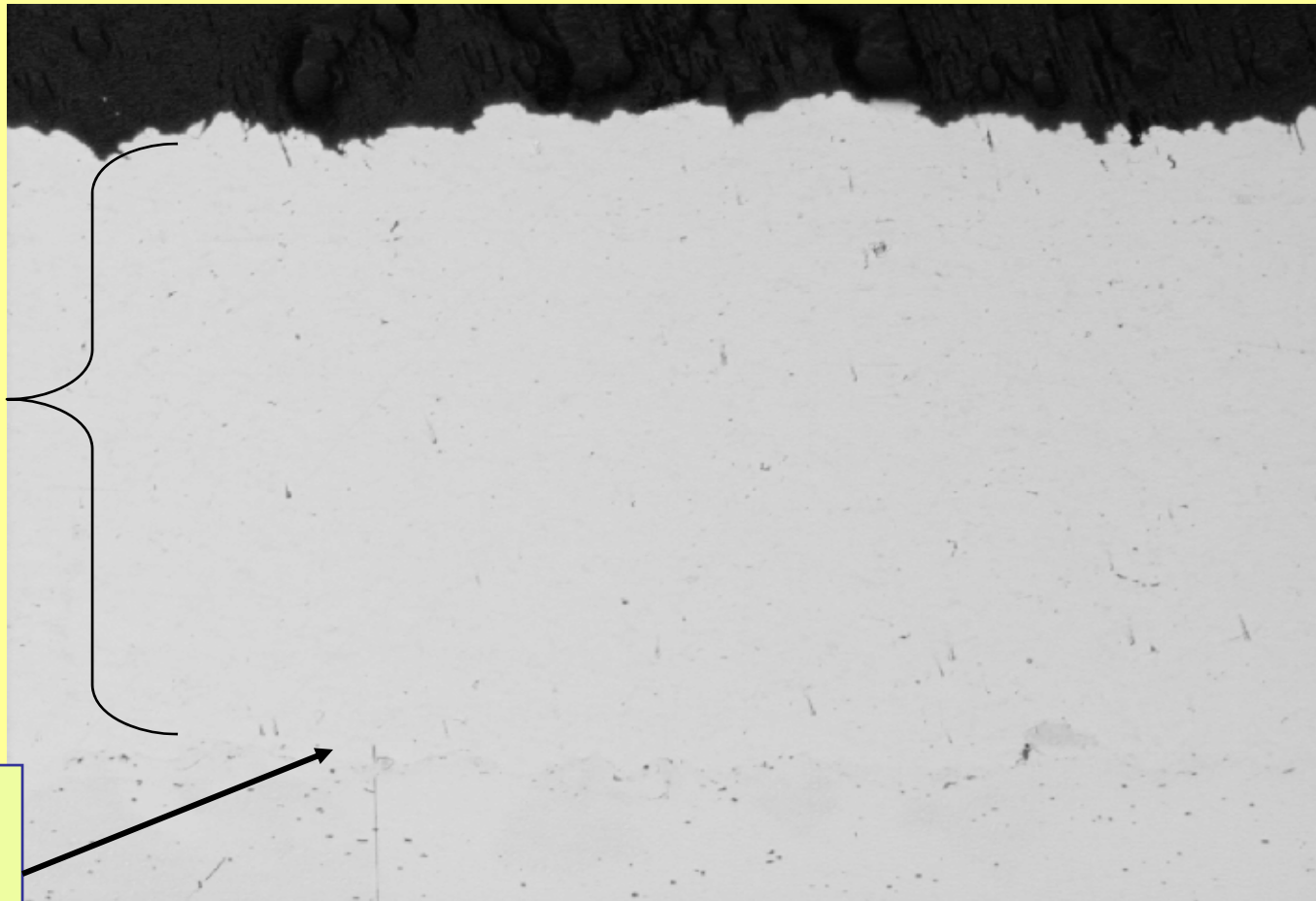




Cold Spray Coating of CP-Al On ZE 41A-Mg (Nitrogen Gas @ 400°C)

Cold
Spray
CP- Al
Coating

Coating /
Substrate
Interface



10,350 psi adhesion (ASTM C-633)



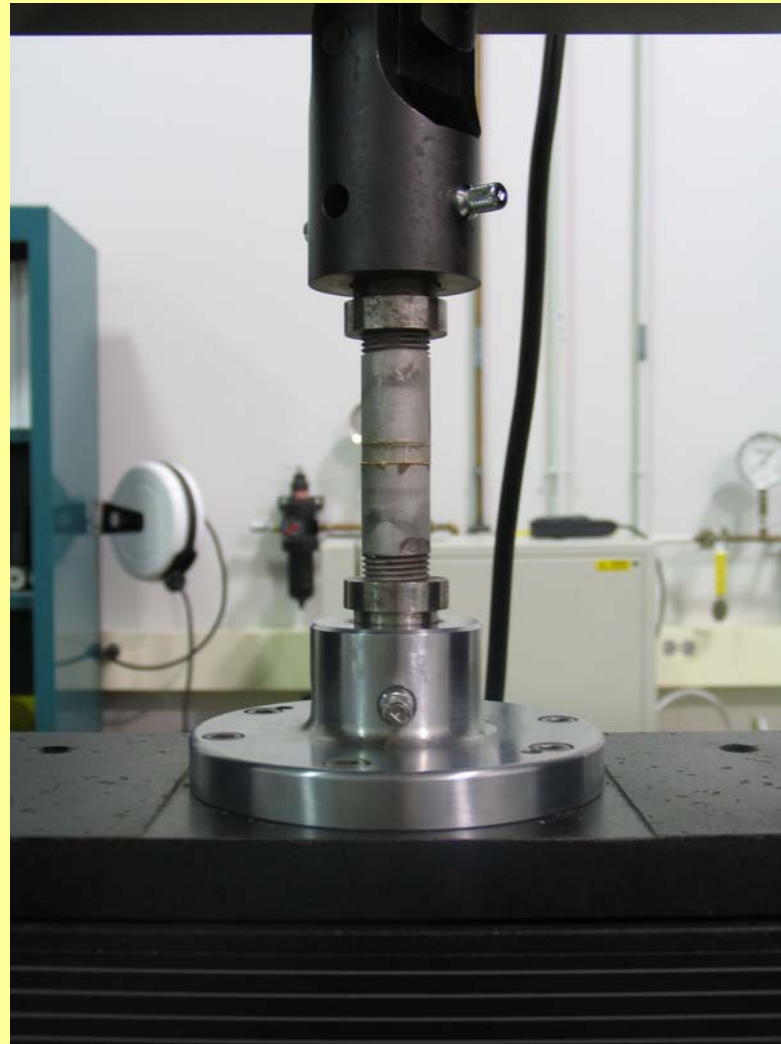
Bond Bar Adhesion Set-up



Bond Strength Measurements on ZE41A Magnesium and 7075 Aluminum Alloy



Bond Bar Adhesion Testing Setup





Results for CP- Aluminum Cold Spray Coatings on 6061 Aluminum Bond Bars

<i>Process Conditions</i>	<i>Nozzle Powder</i>	<i>Adhesion (psi)</i>
N2, 380psi, 250C	Metal 15- 45 um	2743
He, 380psi, 20C	Metal 15- 45 um	1657-3302
N2, 380psi, 300C	Metal/Plastic 7-28 um	2387-4476 (cohesive)
N2, 380psi, 400C	Plastic (125mm) 7-28 um	5787-7247 (cohesive)



Results for CP- Aluminum Cold Spray Coatings on Magnesium

<i>Process Conditions</i>	<i>Nozzle Powder</i>	<i>Adhesion (psi)</i>	<i>Corrosion Results</i>
N2, 380psi, 250C	Metal 15- 45 um	2743	8 hrs
He, 380psi, 20C	Metal 15- 45 um	>8,505 (glue failure)	>500 hrs*
N2, 380psi, 300C	Metal/Plastic 7-28 um	4764-5985	1000 hrs
N2, 380psi, 400C	Plastic 7-28 um	>10,350 (glue failure)	>2,400 hrs*

*** Failure of Edge Maskant**



Salt Spray (Fog) Corrosion Test (ASTM B-117)



- Specimens at 15-30° angle from vertical
- 5 +/- 1% (by weight) NaCl Solution (pH 6.5-7.2)
- Spray Nozzle Baffled at 10-25psi
- Chamber Temperature at 35 + 1.1 – 1.7 °C
- Continuously sprayed in closed chamber

Note: No Direct Relation between B117 & Outdoor Exposure



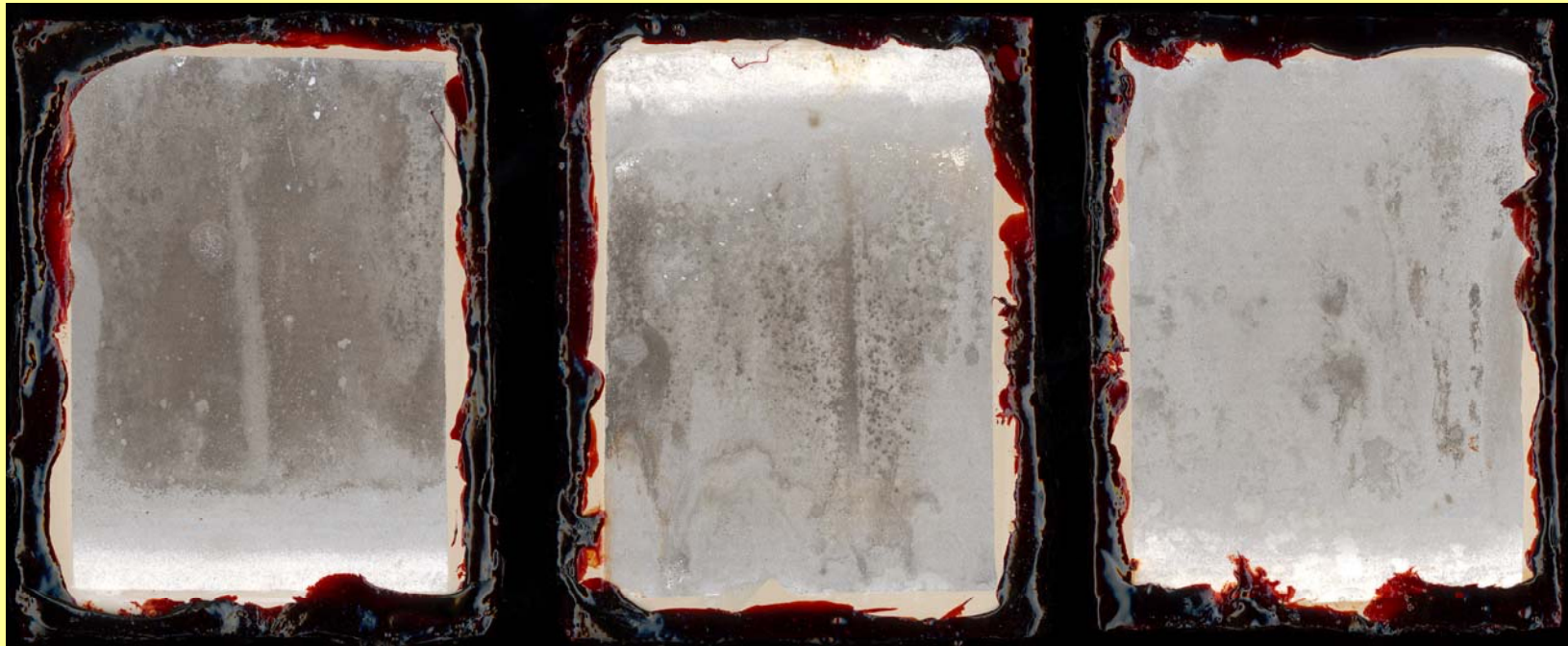
Aluminum coated ZE41A Magnesium (8 Hours in Salt Spray)



Cold Spray Aluminum deposited using N₂ Gas at 250 °C



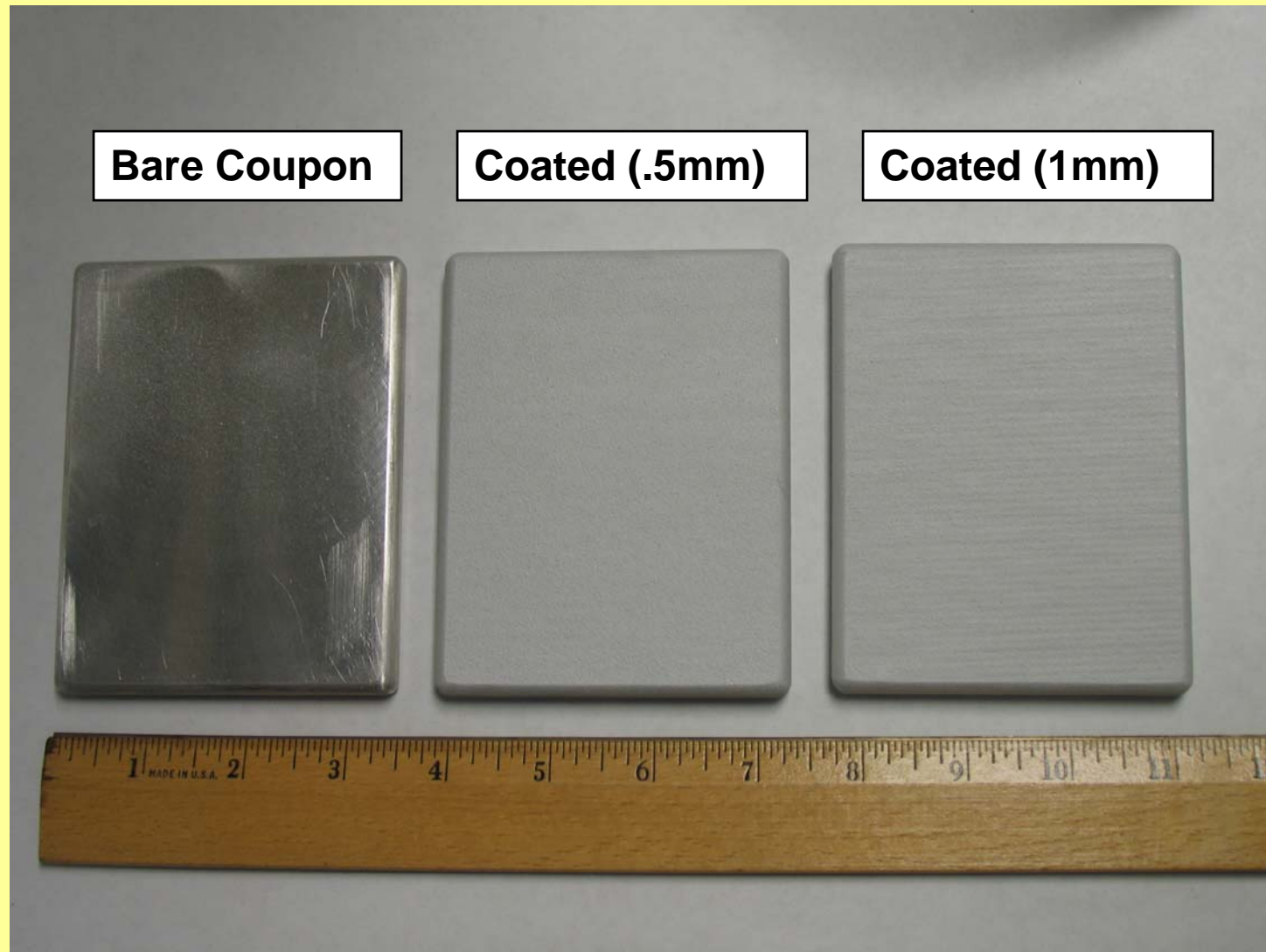
Aluminum coated ZE41A Magnesium (336 Hours in Salt Spray)



Cold Spray Aluminum deposited using Helium Gas at 20 °C



Cold Spray Aluminum coated ZE41A Magnesium Coupons



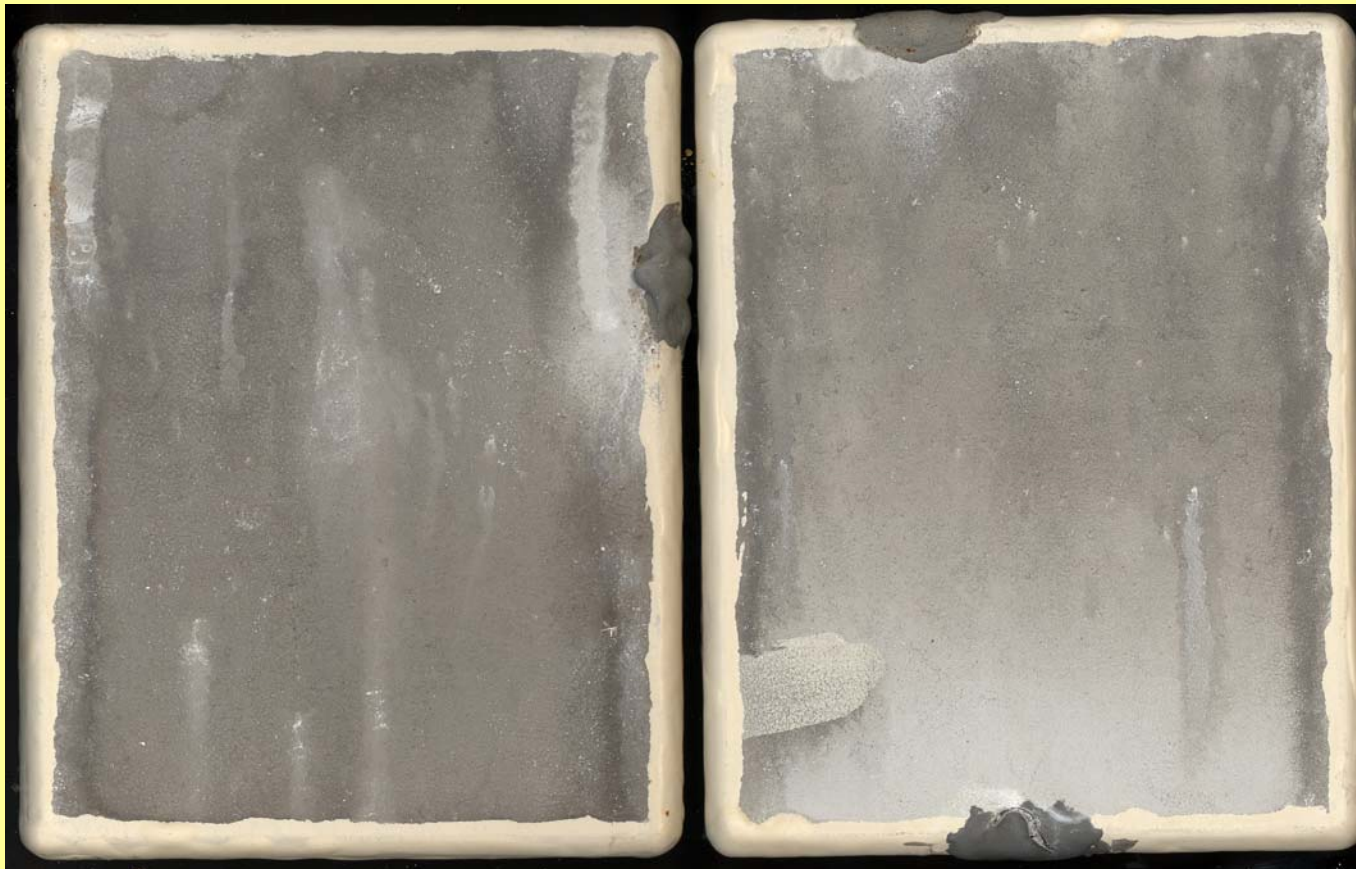


Aluminum Cold Spray Coated Magnesium Coupons After Salt Spray Exposure



2400 Hours Exposure (.5mm)

2400 Hours Exposure (1mm)



Cold Spray Aluminum deposited using N₂ Gas @ 400 °C



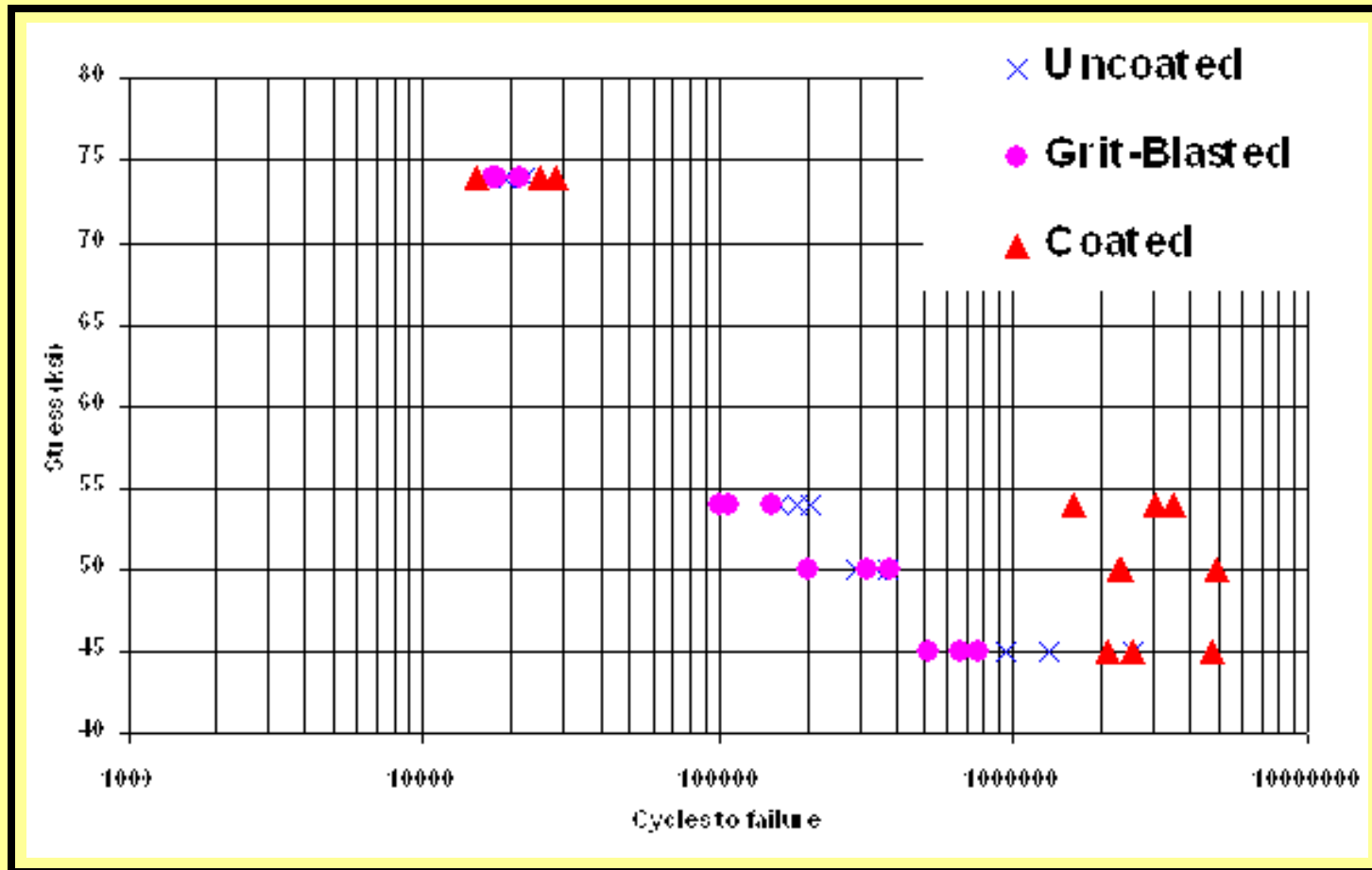
RCB Cold Spray Set-Up



ZE41A Magnesium & 7075 Aluminum Alloy RR Moore Fatigue Specimens



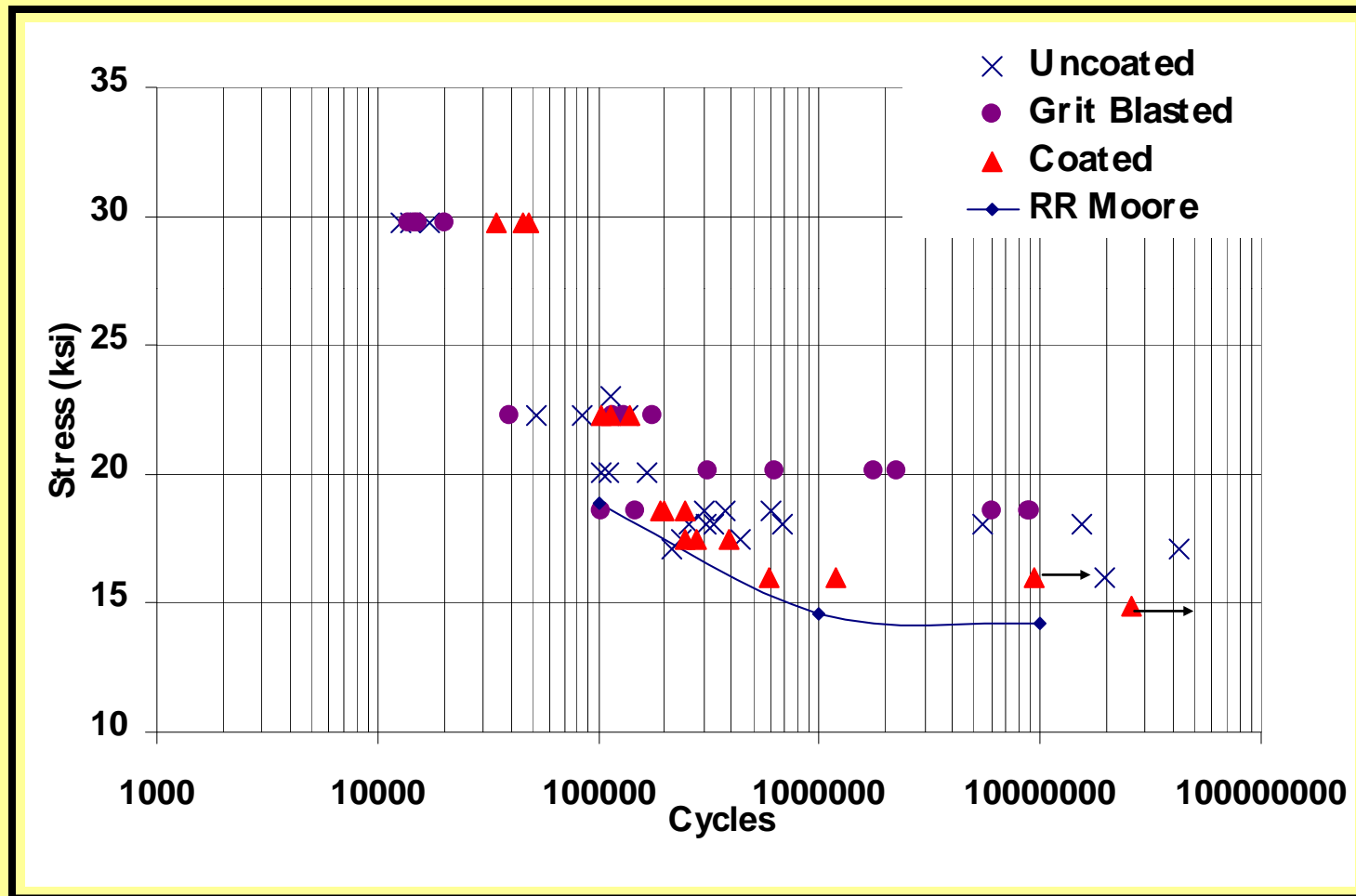
Fatigue Results – AA7075-T651



Source – Australian Defence Science & Technology Organisation



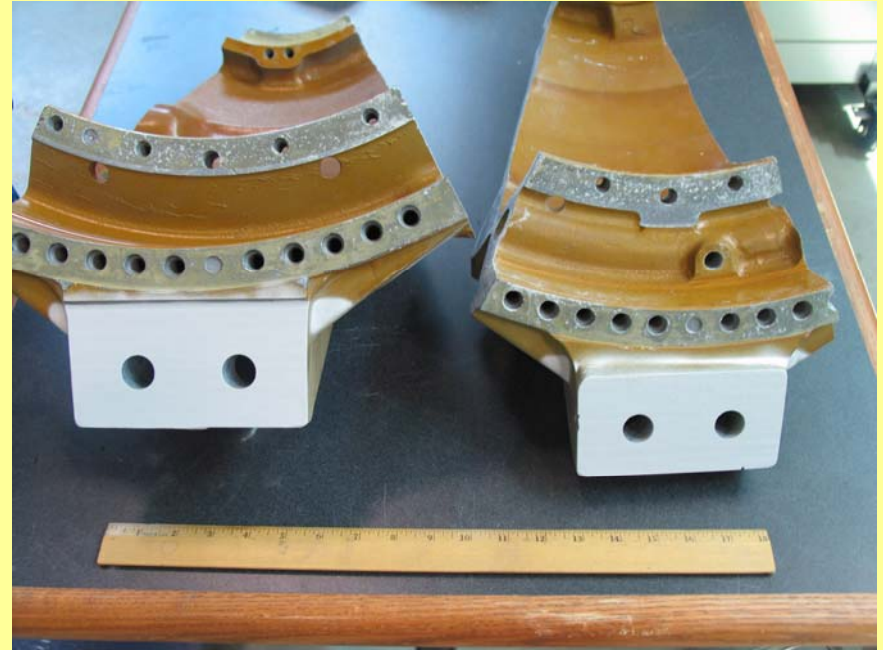
Fatigue Results – ZE41A-T5



Source – Australian Defence Science & Technology Organisation



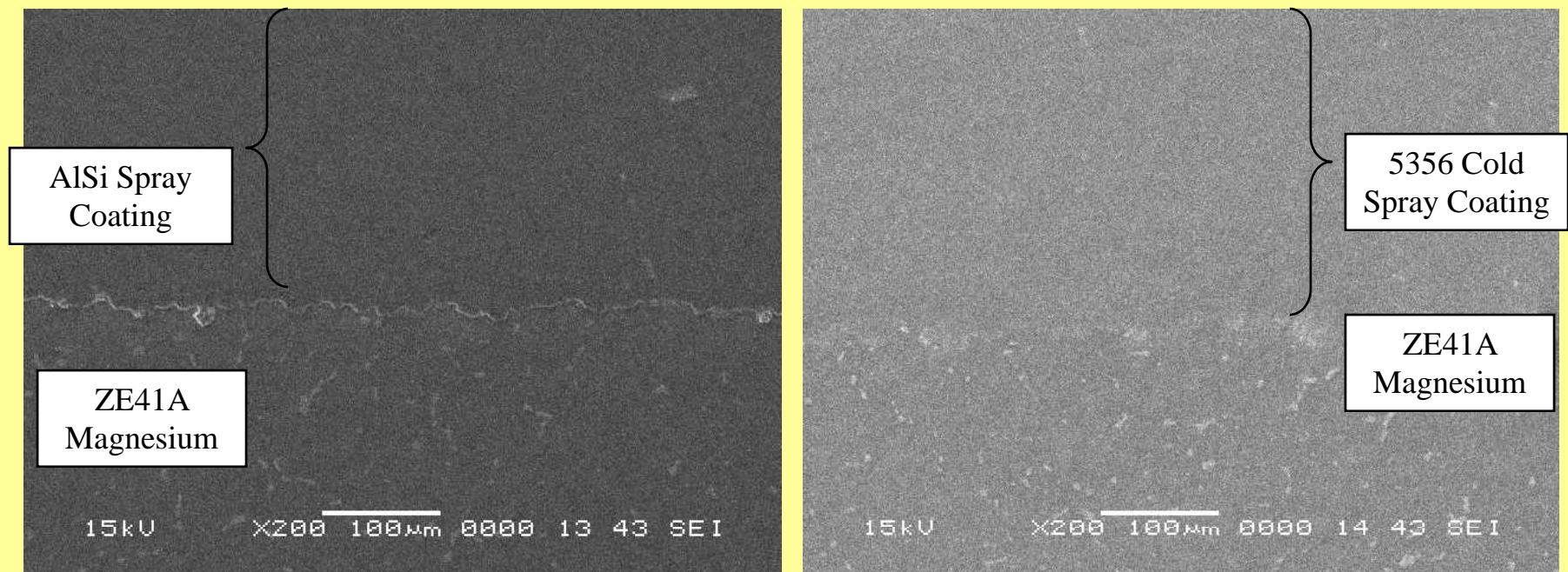
Mg Housing Coated with CP-Al



Flat surface of Mg housing covered with CP-AL Cold Spray



Al12Si & 5356 Al Deposited on ZE41A Using Helium



Adhesion Results - > 8,000 psi (Glue Failure)



Summary

Achieved High Density, Low Porosity Cold Spray Aluminum Coating

Bond Strength Exceeds 10,000 psi.

Corrosion Resistance exceeds 2500 hours B117 Salt Fog Spray

No Reduction in Fatigue Strength on Magnesium

Slight fatigue credit on 7075 Aluminum Alloy

Future Work – Investigate Aluminum Alloys & High Purity Aluminum